

Nonlinear Behavior of Josephson Traveling Wave Parametric Amplifiers

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Abstract—Recent advancements in quantum technologies and advanced detection experiments have underscored the pressing need for the detection of exceedingly weak signals within the microwave frequency spectrum. Addressing this challenge, the Josephson Traveling Wave Parametric Amplifier (JTWPA) has been proposed as a cryogenic front-end amplifier capable of approaching the quantum noise limit while providing a relevant bandwidth. This research is centered on a comprehensive numerical investigation of the JTWPA, without resorting to simplifications regarding the nonlinearity of the essential components. Specifically, this study focuses on a thorough examination of the system, characterized by coupled nonlinear differential equations representing all components of the device. Proper input and output signals at the device's boundaries are considered. The analysis of the output signals undergoing the parametric amplification process involves a detailed exploration of phase-space dynamics and Fourier spectral analysis of the output voltage. This study is conducted while considering the parameters ruling the response of the device under pump and signal excitations. In addition to the expected signal amplification, the findings reveal that the nonlinear nature of the system can give rise to unforeseen phenomena, depending on the system's operational conditions, which include: the generation of pump tone harmonics, modulation of the signal gain, and incommensurate frequency generation—effects that are not easily accommodated by simplistic linearized approaches.

Index Terms—Josephson junctions, Josephson travelling wave parametric amplifiers, microwave amplifiers, parametric amplifiers, superconducting microwave devices.

I. INTRODUCTION

NOWADAYS, there has been considerable interest in superconducting quantum limited parametric amplifiers due to

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their relevance in various practical applications, e.g., quantum optics [1], [2], quantum measurement [3] qubit readout [4], and microwave single photon detection [5], [6], [7], [8], [9], [10]. Many of these applications involve the simultaneous multiple reading and the utilization of multiplexing strategies, needing large bandwidth amplifiers with minimal noise.

Quantum limited parametric amplifiers offer a clear advantage by providing substantial amplification while enabling the possibility of approaching and, in some cases, surpassing the quantum noise limit under specific conditions [11].

The fundamental principle of parametric amplification hinges on the generation of frequency mixing induced by the system nonlinearity. Practically, it entails the amplification of a weak signal through its interaction with a more robust pump tone, leading to a pump-to-signal energy transfer. The implementation of these devices frequently needs Josephson junctions (JJs), which, due to their nonlinear inductance, act as tunable nonlinear resonators, thus allowing adjustment of the resonance frequency to achieve optimized amplification.

II. JTWPA

Josephson parametric amplifiers (JPAs) achieve power transfer from a robust pump tone to a weak signal through the inherent non-linearity of the JJ and a subsequent frequency mixing process. The interested reader can find a comprehensive review of recent JPAs developments in [12]. It's worth noting that, while JPAs can approach the quantum noise limit, they exhibit limitations in terms of bandwidth, dynamic range, and linearity [12], [13]. In particular, the limited bandwidth of JPAs restricts their feasibility. For instance, in applications like qubit readout, the capacity to read a few qubits per amplifier is a bottleneck in scaling up quantum processors [14], [15]. Additionally, in axion detection experiments, scaling the setup to include a series of cavities is not feasible [16], [17], [18].

In contrast, superconducting Traveling Wave Parametric Amplifiers (TWPAs) maintain a low quantum noise level while offering a broad bandwidth. Although the theoretical framework for these amplifiers is relatively aged [19], [20], they are currently experiencing a resurgence in popularity, with frequent new proposals and implementations emerging. Superconducting TWPAs operate by parametrically amplifying microwaves

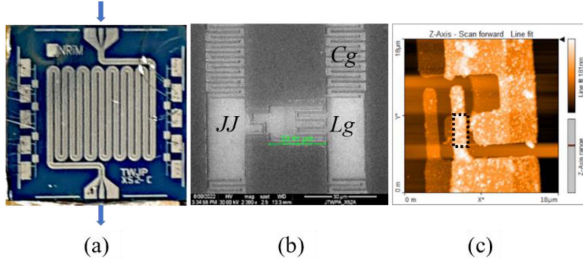


Fig. 1. Realized JTWPA: (a) the whole chip; (b) a SEM photograph of a single cell; (c) an AFM picture of one of the 990 JJs forming the JTWPA.

propagating along a transmission line containing nonlinear components, often realized using JJs. The current-dependent Josephson inductance plays a pivotal role in the parametric mixing and amplification process. By injecting a high-amplitude pump tone at frequency f_{pump} and a weak signal to be amplified at frequency f_{sign} , the large-amplitude pump tone modulates the nonlinear Josephson inductance, facilitating the coupling between the pump and signal. This process may result in signal amplification and the generation of an idle tone, at frequency f_{idle} . Depending on the current dependence of the nonlinearity, two distinct operating regimes emerge: a four-wave mixing (4WM) mode, where the following relation holds: $2f_{pump} = f_{sign} + f_{idle}$, and a three-wave mixing (3WM) mode, where the relation between the involved frequencies is: $f_{pump} = f_{sign} + f_{idle}$, reflecting the conservation of energy in the photon mixing process. The latter mode arises when the nonlinear inductance term exhibits odd dependence on current and is typically obtained by biasing the line with a DC current and/or magnetic field.

This study focuses on the modeling of a specific JTWPA scheme, comprising a series of SQUIDs [21], [22], [23], [24], [25], [26], [27] and a capacitive shunt to ground. Typically, these devices offer nearly quantum-limited noise levels and a wide bandwidth (approximately 6 GHz centered at 7 GHz), albeit with limited gain (<20 dB) and dynamic range (<-90 dBm). For an in-depth description of JTWPAs, please refer to [28], [29].

In Fig. 1 is shown one of the realized JTWPAs, designed and fabricated at INRiM - Italy as part of the DARTWARS project [30], [31], [32], [33], [34]. Fig. 1a shows the whole chip, having lateral size of 1 cm, with the input port for the signal and pump indicated by the inward arrow and the output port by the outward arrow. The ports are connected, through suitable waveguides, to the rest of the amplification chain. The JTWPA is formed by 990 cells in series, each comprising a parallel connection between a JJ and an inductor, forming an rf-SQUID, and a grounding capacitor. These components are indicated by the JJ, L_g , and C_g labels in Fig. 1b. The JJs were realized by e-beam evaporation of an Al/AlOx/Al trilayer using the shadow mask deposition technique. In Fig. 1c is shown an AFM image of one of the fabricated junctions. The junction area is outlined by the dotted rectangle. Typical obtained junction dimensions are $3.8 \mu\text{m}$ by $1.6 \mu\text{m}$.

III. MODELLING

Fig. 2 shows the electric circuit equivalent of the JTWPA analyzed in this study. The gray-shaded section within Fig. 2

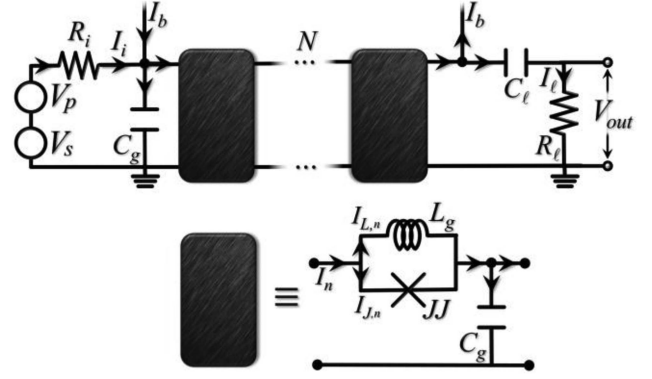


Fig. 2. Equivalent circuit of the analyzed JTWPA composed by N identical replicas of the cell shown at the bottom.

TABLE I
VALUES USED FOR THE PARAMETERS

Name	N	R_i	R_l	C_l	C_g	L_g	R_J	C_J	I_J
units		Ω	Ω	nF	fF	pH	k Ω	fF	μA
value	990	50	50	1	24	120	20	200	2

shows to the generic n^{th} cell within the JTWPA, while the top row delineates left and right boundary elements. The specific parameter values are derived from experimental data [31] and shown in Table I. The arrows represent the injection points of an optional DC bias current I_b used to modulate nonlinearities.

The JTWPA under consideration in this work comprises a series of N identical cells, each housing an rf-SQUID. These cells consist of a JJ in parallel with a geometric inductance L_g and a capacitor C_g to ground. At the initial cell in the chain is applied the voltage of the pump and signal tones, denoted as:

$$V_i(t) = V_p(t) + V_s(t) = V_{pump} \sin(2\pi f_{pump}t) + V_{sign} \sin(2\pi f_{sign}t) \quad (1)$$

through an ideal linear transmission line, modeled by the input resistance R_i . The last chain element sees the load resistance R_l through a capacitor C_l , inserted to block the DC current. The equations governing the behavior of a generic n^{th} cell are:

$$I_n - I_{n+1} = \frac{dq_n}{dt} \quad (2)$$

$$I_n = I_{J,n} + I_{L,n} = I_{J,n} + \frac{\hbar}{2e} \frac{\varphi_n}{L_{g,n}} \quad (3)$$

$$\frac{\hbar}{2e} \frac{d\varphi_n}{dt} + \frac{q_n}{C_{g,n}} = \frac{q_{n-1}}{C_{g,n-1}}, \quad (4)$$

while the boundary conditions can be written as

$$\frac{dI_i}{dt} = \frac{1}{R_i} \frac{dV_i}{dt} - \omega_i (I_i + I_b - I_1) \quad (5)$$

$$\frac{dI_l}{dt} = -\omega_l \left[\left(1 + \frac{C_{g,N}}{C_l} \right) I_l + I_b - I_N \right]. \quad (6)$$

Here: φ is the Josephson phase difference; \hbar and e are the reduced Planck constant and electron charge; q_n is the charge on the capacitor $C_{g,n}$; I_n , $I_{L,n}$ and $I_{J,n}$ are the total, the $L_{g,n}$ and the JJ currents respectively; $\omega_i = 1/(R_i C_g)$

and $\omega_l = 1/(R_l C_{g,N})$. The current $I_{J,n}$ is accounted for by the Resistively and Capacitively Shunted Junction (RCSJ) model [36]:

$$I_{J,n} = C_J \frac{\hbar}{2e} \frac{d^2 \varphi_n}{dt^2} + \frac{1}{R_J} \frac{\hbar}{2e} \frac{d\varphi_n}{dt} + I_c \sin \varphi_n, \quad (7)$$

where I_c the Josephson critical current, and C_J and R_J are the junction capacitance and resistance, respectively.

These values yield a plasma frequency $f_p \approx 27.7$ GHz. The value of R_J is estimated and chosen large enough to not affect the overall dynamics. Using the 2nd Josephson relation, $V = \frac{\hbar}{2e} \frac{d\varphi}{dt}$, the nonlinear inductance of a JJ, $L_J(I)$, for $I < I_c$, is:

$$L_J(I) = \frac{\hbar}{2eI_c} \frac{1}{\sqrt{\left(1 - (I/I_c)^2\right)}} \quad (8)$$

In essence, the bias current serves as a control parameter for tuning the Josephson inductance. As I increases, the inductance grows, eventually diverging for $I \rightarrow I_c$.

Theoretical approaches [36], [37] typically linearize $L_J(I)$ and consider simplified scenarios in lower-order approximations. In contrast, our approach addresses the problem in its entirety by solving a system of N coupled differential equations [26], with appropriate boundary conditions. The system's dynamics are obtained by integrating these N coupled differential equations using a finite-difference implicit method based on a tridiagonal algorithm, often used for numerical studying Josephson transmission lines [38], [39], [40]. The output signal is analyzed in its spectral components using an algorithm based on Mathematica software. The chosen values for the normalized time step and integration time are $\Delta t = 0.01$ and $t_{\max} = 20000$, respectively, corresponding to $\Delta t = 0.06$ ps and $t_{\max} = 120$ ns. This allows to integrate for a sufficient time to rule out transient phenomena while preserving stability of the integrator. The chosen methodology enables to analyze the complete signals in the time and frequency domains, the effect of each system parameter on the device performances, the effect of spatial changes of the parameters due to the imperfections that affect practical realization of devices, and the effects induced by intrinsic thermal noise. In this work, identical cells for the JTWPA are assumed. The effects of parameter value distributions [41] and of thermal noise will be explored in future work. Next sections present numerical integration results involving the JTWPA operating in 4WM mode, and analyze the effects of pump power, signal frequency, and of the variation of the transmission line parameters on the overall dynamics and, more specifically, on the amplifier gain.

IV. RESULTS

Fig. 3 shows two examples of Fourier spectra of output voltage by fixing the pump frequency to 7 GHz and the input signal power to -100 dBm. Fig. 3(a) shows the output spectral power densities (in intensity scale) resulting by sweeping the pump power from -70 to -50 dBm and with $f_{\text{sign}} = 6.42$ GHz.

The pump, signal, and idle peaks, and their harmonics, are clearly visible for all pump powers. Three regions are evident in the spectra, as also discussed in Ref. [42]:

- 1) $P_{\text{pump}} < -57$ dBm: a moderate gain (< 5 dB) is obtained.
- 2) $P_{\text{pump}} \in [-57, -54]$ dBm: the signal gain increases up to ~ 10 dB, as well as the number of visible harmonics.

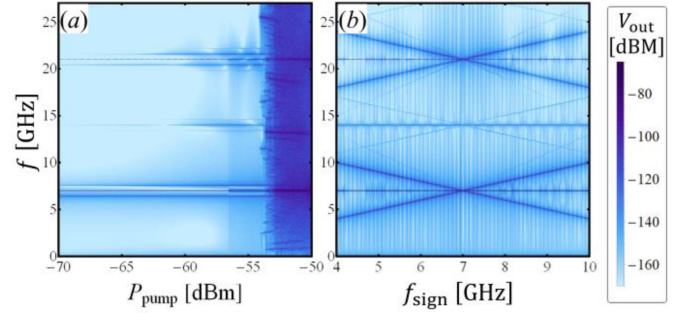


Fig. 3. Fourier spectra of the output voltage versus the pump power level for $f_{\text{sign}} = 6.42$ GHz (a) and versus the signal frequency for $P_{\text{pump}} = -55$ dBm (b). The color intensity scale represents the amplitude of the spectral components whose frequency can be read on the left vertical axis. The pump frequency is 7 GHz and the input signal power is -100 dBm.

- 3) $P_{\text{pump}} > -54$ dBm: the apparent gain is large, but the system enters a turbulent regime with a large noise rise at all f_{sign} .

Last situation, caused by the overly intense pump power, is certainly not suitable for an amplifier. Consequently, there is a limit to the maximum power available for amplification. It is worth nothing that this effect can be only seen from the numerical simulation of the full nonlinear system dynamics.

Fig. 3(b) displays the output spectra obtained by setting $P_{\text{pump}} = -55$ dBm, corresponding to the average “clean” gain region, and sweeping f_{sign} from 4 GHz to 10 GHz. The peaks corresponding to the pump, signal, and idle are clearly visible in all frequency range, with their first and second harmonics, denoting the large bandwidth of the amplifier. Also, some other lines are visible, corresponding to different combinations between the involved frequencies. These signals subtract power from the signal to be amplified and can generate instability. The vertical bands visible in Fig. 3(b) are due to gain ripples, which is discussed in more details in the following.

Fig. 4(a) shows the gain vs frequency response of the amplifier, when operated in the “clean” gain region, that is with $f_{\text{pump}} = 7$ GHz, $P_{\text{pump}} = -55$ dBm and $P_{\text{sign}} = -100$ dBm. All the other system parameters are as reported in Table I. The so-called “ripples” in the gain profile are clearly visible, see the inset. They are due to variable impedance along the transmission line that do not well matches the input and output impedances and generate interference between forward and backward propagating waves undergoing multiple reflections [41], [43]. These ripples have been described as Fabry-Pérot-like resonances [26], [44] with a bandwidth inversely proportional to the waveguide length. Recently, an approach based on the theory of coupled modes [36], successfully predicts the formation of these ripples by considering the interactions of reflected waves [45]. In the investigated scheme, the emerging ripple pattern depends on parameter values and profoundly affects both the gain and bandwidth of the device.

To better clarify this effect, in Fig. 4(b)–(d) the gain response has been computed by varying the system parameters. Fig. 4(b) and (c) are obtained by setting C_g to 16 pF and 32 pF, respectively. A larger capacitance to ground increases the average gain, but also increases the number of ripples and reduces the bandwidth. Moreover, a further increase of the capacitance triggers a chaotic system response (data not shown). Fig. 4(d) illustrates

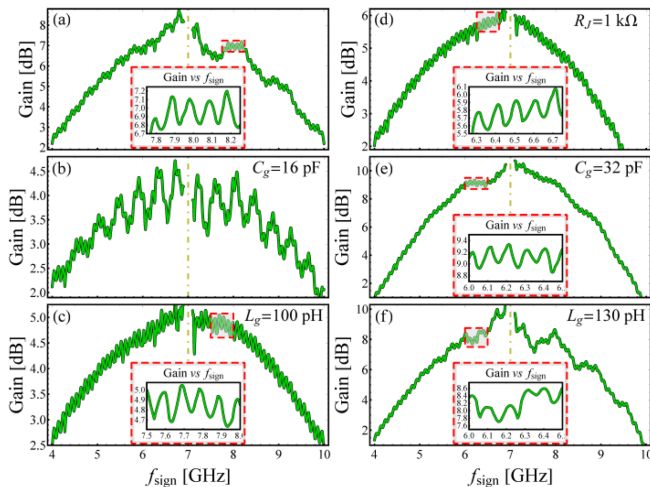


Fig. 4. Frequency response of the JTWPA and effect of change of parameters. The signal power is fixed to -100 dBm, the pump frequency to 7 GHz, and power to -55 dBm. The insets detail the gain ripples. The parameters in (a) are as in Table I, while in other panels only one parameter value changes from this table, i.e., (b) $C_g = 16$ pF, (c) $C_g = 32$ pF, (d) $R_J = 1$ kΩ, (e) $L_g = 100$ pH, and (f) $L_g = 130$ pH.

what happens when decreasing R_J from 20 kΩ to 1 kΩ, i.e., increasing the dissipation being the damping parameter equal to $\alpha = 1/(R_J C_g f_p)$. A significant reduction of the gain is evident, although it is fair to point out that at the usual working temperatures of JTWPAs, i.e., a few tens of mK, such small resistances are unrealistic. Fig. 4(e) and (f) shows effects of changing the loop inductance L_g to 100 pH and 130 pH, respectively. In the former case a suppression of ripples is obtained, together with a reduction in average gain, while in the latter case higher gains are achieved, but at the cost of instability in the higher-gain regions.

V. CONCLUSION

JTWPA are promising superconducting devices for wide-band ultra-weak signal amplification in the microwave spectral region. Semi analytic and simple numeric approaches, based on approximations in the nonlinearity and on limited frequency components, can reproduce most but not all the experimental features. Using a direct numerical simulation of the complete system, it has been shown that, beside the expected signal amplification and depending on the system operation, unwanted effects emerge (such as pump tone harmonics, incommensurate frequency generation, and ripple formation in the gain profile), which are not easily accounted for in simpler approaches. Moreover, the impact of the main system parameter on the response of the system has been investigated, making it possible to establish “threshold” values below which chaotic effects, detrimental to use as an amplifier, can be safely avoided.

Next steps will be investigation of 3WM and RPM configurations to closely reproduce experimental results and understand sources of nonidealities. The effects of intrinsic fluctuations in JJs, which are important in determining their switching [46], [47], [48], and their combined effect with the nonlinear dynamics will also be addressed as possible source of additional noise. Moreover, other schemes can be explored, for instance including two JJs in parallel in the rf-SQUID to achieve higher operation frequencies in “optical modes” [49].

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