

## Manuscript Details

<b>Manuscript number</b>	YBENG_2017_969
<b>Title</b>	Drying rate control in microwave assisted processing of sliced apples
<b>Article type</b>	Research Paper

### Abstract

The most enhanced systems perform microwave related drying of fruits and vegetables by continuously adjusting the power level in order to maintain the product temperature over a target value. As a result, typical drying curves are followed which exhibit fast drying rates in the middle stage. That can often lead to quality damage or undesirable changes in the food colour and texture. In response to these issues, a microwave system able to realize apples drying processes by keeping constant evaporation rates is proposed. This approach requires a continuous temperature adjustment of the apple slices under test, whose thermal level is detected by computer aided infrared thermography system. Since temperature corrections are required only during the middle stage of the process, the overall drying time is only slightly affected by the proposed control strategy. Nevertheless, compared to microwave drying with different constant temperatures: 60, 70 and 80°C, the resultant benefits operating at constant evaporation rates, include an improvement of texture and rehydration properties, while no differences in colour of sliced apples were observed.

<b>Keywords</b>	microwave; drying; infrared thermography; apple; color; texture
<b>Manuscript region of origin</b>	Europe
<b>Corresponding Author</b>	luciano cinquanta
<b>Corresponding Author's Institution</b>	University of Molise
<b>Order of Authors</b>	gennaro cuccurullo, Laura Giordano, Antonio Metallo, luciano cinquanta
<b>Suggested reviewers</b>	Reza Amiri Chayjan, S.N. Karaaslan

## Submission Files Included in this PDF

### File Name [File Type]

Highlights.docx [Highlights]

GraphAbs.docx [Graphical Abstract]

MW\_Apple\_2017.docx [Manuscript File]

Figure 1 - Schematic.tif [Figure]

Figure 2-Drying curves.tif [Figure]

Figure 3-Drying rate curves.tif [Figure]

Figure 4 - The fundamental mapping .tif [Figure]

Figure 5 - Constant temperature tests.tif [Figure]

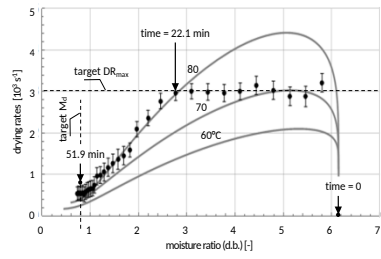
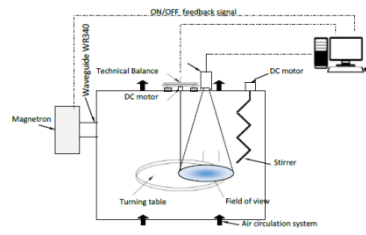
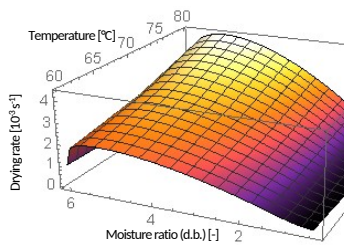
Figure 6 - Control of the drying rate.tif [Figure]

Figure 7 - Maximum and average surface temperature evolution.tif [Figure]

To view all the submission files, including those not included in the PDF, click on the manuscript title on your EVISE Homepage, then click 'Download zip file'.

## **Highlights**

- A microwave system with constant evaporation rate was developed for apples drying.
- Constant evaporation rate operations helped to reduce product hotspots.
- Constant evaporation rate did not affect the color of microwaved dried apples
- Microwave drying with constant evaporation rates seems to improve apples texture



1 **Drying rate control in microwave assisted processing of sliced apples**

2  
3 *Gennaro Cuccurullo <sup>a</sup>, Laura Giordano <sup>a</sup>, Antonio Metallo <sup>a</sup>, Luciano Cinquanta <sup>b,\*</sup>*

4  
5 <sup>a</sup> Dipartimento Ingegneria Industriale, University of Salerno, Italy

6  
7 <sup>b</sup> Dipartimento Scienze Agrarie, Alimentari e Forestali, University of Palermo, Italy

8  
9 \*corresponding author. Luciano.Cinquanta@gmail.com

10 **Key words:** microwave; drying; infrared thermography; apple; color; texture

11

12

13

14 **Abstract.** The most enhanced systems perform microwave related drying of fruits and  
15 vegetables by continuously adjusting the power level in order to maintain the product  
16 temperature over a target value. As a result, typical drying curves are followed which  
17 exhibit fast drying rates in the middle stage. That can often lead to quality damage or  
18 undesirable changes in the food colour and texture. In response to these issues, a microwave  
19 system able to realize apples drying processes by keeping constant evaporation rates is  
20 proposed. This approach requires a continuous temperature adjustment of the apple slices  
21 under test, whose thermal level is detected by computer aided infrared thermography  
22 system. Since temperature corrections are required only during the middle stage of the  
23 process, the overall drying time is only slightly affected by the proposed control strategy.  
24 Nevertheless, compared to microwave drying with different constant temperatures: 60, 70  
25 and 80°C, the resultant benefits operating at constant evaporation rates, include an  
26 improvement of texture and rehydration properties, while no differences in colour of sliced  
27 apples were observed.

28

29

30

31

32

33 **Symbols and abbreviations**

Symbol or abbreviation	Unit	Meaning
MW		microwave
IR		infrared
EM		electromagnetic
RMSE		root mean square error
d.b.		dry basis
i.d.		internal diameter
o.d.		outside diameter
$M_d(t)$	-	moisture content on dry basis
$m_{\text{water}}(t)$	kg	moisture content at time t
$m_{\text{dry}}$	kg	dry mass
$DR(t)$	s <sup>-1</sup>	drying rate
$DR_{\text{max}}$	s <sup>-1</sup>	target value of $dr(t)$
$a$	s <sup>-1</sup>	equation fitting coefficient
$b$	s <sup>-c-1</sup>	equation fitting coefficient
$c$	-	equation fitting coefficient
$d$	s <sup>-e</sup>	equation fitting coefficient
$e$	-	equation fitting coefficient
$\Gamma(\beta, z) = \int_z^{\infty} t^{\beta-1} e^{-t} dt$		incomplete gamma function
$T_{\text{max}}$	[°C]	maximum surface temperature
$t_{\text{max}}$	s	time for which $M_d = 0.8$
NEB		non enzymatic browning
$WI = \frac{100 - \sqrt{(100 - L^*)^2 + a^{*2} + b^{*2}}}{b^{*2}}$		white index
34 $L^*$		brightness
35 $a^*$		red index
36 $b^*$		yellow index

37

38

39 **1. Introduction**

40 Over the last decades, attractive results arising from microwave (MW) heating led to  
 41 develop several techniques to control temperature level. It is well known that realizing MW  
 42 assisted drying under appropriate processing conditions can increase speed of operation;  
 43 improve fruit food quality, such as colour and texture, while reducing energy consumption  
 44 (Gunasekaran, 1999). Researchers have studied various microwave power control profiles  
 45 in order to meet consumer expectations by high quality food products, thus, intermittent  
 46 methods and continuous methods have been proposed, most of them based on keeping

47 power density or temperature under control (Zhenfeng, Wang, Raghavan & Cheng, 2006;  
48 Cuccurullo, Giordano, Metallo & Cinquanta, 2017).

49 Operating at constant power rates determines unuseful temperature increases in the early  
50 stage; meanwhile it causes undesirable changes in quality, such as browning of fruit surface  
51 colour and charring (Raghavan, Zhenfeng, Wang & Gariépy, 2010; Zhenfeng, Raghavan,  
52 Wang & Vigneaultd, 2011). According to Clark (1996) and Nijhuis et al. (1998), excessive  
53 temperatures along the edges and corners of products may lead to overheating and  
54 irreversible drying-out resulting in possible scorching and development of off-flavours.

55 Drying of fruit at constant temperature usually implies a typical drying curve is followed  
56 featured by rapid evaporation in the middle stage. In general, a complete MW drying is  
57 featured by three drying periods: I) heating-up period, in which the temperature of the  
58 product increases with time and the material starts to lose moisture at relatively small rates;  
59 II) middle stage drying period, during which a stable temperature profile is established and  
60 drying rates are highest; III) falling rate period, during which drying rates progressively  
61 slow down.

62 One of the major drawbacks of this control strategy is that too rapid mass transport by MW  
63 power may cause quality damage or undesirable changes in the food texture (Koné et al.  
64 2013). Therefore, a suitable and adjustable temperature level or energy density should be  
65 set in order to encompass the opposite requirements: product quality, time and energy  
66 consumptions. In this framework, Raghavan et al. (2010) developed a microwave drying  
67 system, which allowed linearizing the drying curve in the middle stage; to this purpose, the  
68 power level was varied thus reducing product temperature, which was online recorded by  
69 a fibre optic sensor. Some researchers (Zhenfeng et al. 2006; Zhenfeng et al, 2011)  
70 presented an evolution of this system, which was based on a fuzzy logic control able to  
71 adjust the drying curves by monitoring volatiles emanating from carrots during drying.

72 In the present paper, a control system able to slow down the drying rate in the middle stage  
73 of the drying process is designed in order to keep the drying rate at a constant value. The  
74 developed system adjusted continuously the drying temperature depending on the actual  
75 moisture content and on the target temperature level of the apples slices under test. At this  
76 aim, an infrared camera looking at the surface samples temperatures was used to set the  
77 magnetron delivered power. Then, a relationship among temperature, drying rate and  
78 moisture content of the samples was established by suitable data processing based on a  
79 preliminary characterization of their drying kinetics. Five parameters fitting curve was

80 introduced able to fairly adapt samples behaviour during all the stages of the drying  
81 process, whereas typical data fitting involves the falling rate period. The quality of the dried  
82 apples was assessed by colour and texture analysis, as well as rehydration capacity.

## 83 **2. Materials and method**

### 84 *2.1 Microwave prototype*

85 Drying experiments were carried out using a Lab scale MW plant (Figure 1), which houses  
86 a magnetron with a nominal power output of 2 kW operating @ frequency of 2.45 GHz.  
87 The reverberating chamber was a metallic cubic room (1m<sup>3</sup>) equipped with a fan placed on  
88 the bottom of the cavity for continuous air renewal. Fresh air was introduced in the chamber  
89 at constant rate and temperature (25°C room temperature). A stirrer was placed inside the  
90 oven to improve heating uniformity (Cuccurullo et al., 2017; Zhenfeng, Raghavan & Wang,  
91 2010). A Teflon rotating annulus (500 mm i.d., 550 mm o.d.) held a high-density  
92 polyethylene squared grid (10 mm x 10 mm), which supported the samples to be tested.  
93 The grid was connected to a technical balance (Gibertini EU-C 1200 RS, Novate Milanese,  
94 Italy) located on the top of the oven for online measuring moisture loss; the acquisition rate  
95 was 120 samples per minute.

96 An infrared (IR) thermometry system (ThermaCAM Flir P65, Canada) looked at the  
97 surface temperatures of the samples through a square hole (70 mm x 70 mm) realized on  
98 the oven top surface. The hole was properly shielded with a metallic grid, which allowed  
99 the IR radiation from the detected scene to escape but entrapping the microwaves (Li et al.,  
100 2010). A specifically realized LabView ® software was employed for acquiring the  
101 feedback signal produced every 0.9 s by the IR equipment. Then, the code allowed  
102 switching on-off the magnetron delivered power through an I/O board (AT MIO 16XE50,  
103 National Instruments, Assago, Italy). The actual temperature level was then adjusted  
104 according to the actual moisture ratio measurements, as shown in paragraph 2.3.

### 105 *2.2 Samples preparation*

106 Fresh apples (*Golden delicious*) were purchased from a local market and stored at 4°C  
107 before drying. Apples were cut into slices (10±0.2 mm thick, 20±0.3 mm diameter) using  
108 a sharp edged stainless steel pipe. The average initial moisture content of the samples was  
109 about 86 ± 0.7%, as resulted by heating samples in a convective oven with air at 105 °C,  
110 until a constant weight. Slices were placed on the support grid suspended in the MW oven

111 (Figure 1). The total applicator load was 200 g. All experimental tests were performed in  
112 triplicates.

### 113 2.3 Data acquisition and reduction

114 A suitably developed LabView 7.1 (National Instruments Corp., Austin, Texas) code was  
115 realized for both data acquisition/reduction and to control the magnetron delivered power.  
116 Data on exhaust air temperature and humidity, instantaneous sample weight were collected  
117 as well. Moreover, the code acquired the samples surface radiosity map as detected by the  
118 IR camera and converted it into temperature values. The camera was calibrated as  
119 previously reported (Cuccurullo, Giordano, Albanese, Cinquanta & Di Matteo, 2012). A  
120 number of samples, corresponding to about 30% of the total, were gathered in the IR scene  
121 every 0.9 s. Because of the turntable rotation, different random samples were detected when  
122 analysing different images.

123 Preliminary experimental tests were carried on by maintaining the surface temperature  
124 level of the samples under test at different target values, i.e. 60, 70 and 80 °C. The code,  
125 after extracting the maximum samples surface temperature from the IR images at time  $t$ ,  
126 compared it to the corresponding set point to realize the required on/off operation. The end  
127 of the experimental tests was conventionally determined when the moisture content on dry  
128 basis

$$129 \quad M_d(t) = \frac{m_{water}(t)}{m_{dry}} \quad (1)$$

130 reached a residual value of 0.8, (Figure 2). The latter target value is selected such as the  
131 uncertainty related to samples actual weight ( $\pm 0.1$  g) determines the end of the test with  
132 an error less than 30 seconds. Then, after performing a polynomial regression of the  
133 experimental data to smooth out short-term fluctuations, each two minutes the  
134 corresponding drying rates curves were calculated evaluating the analytical derivative

$$135 \quad DR(t) = \frac{1}{m_{dry}} \frac{dm_{water}(t)}{dt} \quad (2)$$

136 The experimental sets of (DR,  $t$ ) were fitted by the empirical model

$$137 \quad DR(t) = a - b t^c \exp(-d t^e) \quad (3)$$

138 where the five constants  $a-e$  are equation-fitting coefficients, DR is expressed in  $s^{-1}$  and  $t$   
139 in minutes. The mathematical structure of the previous equation allowed shaping the drying  
140 behaviour typically featuring MW drying during the whole process (Figure 3). In fact, it



141 was observed (Maskan, 2000; Wang, Xiong & Yu, 2004; Chayjan & Alaei, 2013;  
 142 Cuccurullo et al. 2017) that curves are featured by a short “warming up period” after which  
 143 slowing down evaporating rates are progressively realized until a slope inversion takes  
 144 place to smoothly recover the falling rate behaviour. The addressed trend is probably due  
 145 to the different thermal history featuring each individual slice because of the uneven  
 146 temperature field in the EM cavity. Unlike traditional drying, where empirical models work  
 147 only in the falling rate period (Karaaslan & Tuncer, 2008), such a behaviour allows the  
 148 proposed fit to be extended to the whole drying process: the fit satisfyingly recovers the  
 149 experimental trend; the related coefficients and the Root Mean Square Error (RMSE) are  
 150 reported in Table 1. Here, the times needed to complete the drying tests are reported as  
 151 well.

152 The availability of eq. (3) allows retrieving coherently the fitting curve for the experimental  
 153 sets ( $M_d$ ,  $t$ ); integrating the previous equation and imposing the initial condition,  $M_d(t=0)$   
 154 = 6.14 yielded:

$$155 \quad M_d(t) = a t - (b/d) c^{-\frac{1+e}{d}} \Gamma(k, c t^d) + (b/d) c^{-\frac{1+e}{d}} \Gamma(k, 0) + M_{d0}; \quad k = \frac{1+e}{d} \quad (3)$$

156 where  $\Gamma(a, z)$  is the incomplete gamma function. Since the measured moisture ratio decay  
 157 appears smooth and regular, the related fitting seems to be satisfying, (Figure 3); the  
 158 resulting RMSE for the  $M_d$  are given in Table 1. By eliminating the time variable from the  
 159 two previous data set, the measured drying rates were written as function of the  
 160 instantaneous moisture content for each of the three selected temperatures (DR,  $M_d$ ). A  
 161 linear interpolation among the above curves was made to explicitly obtain the “fundamental  
 162 mapping”, that is maximum surface temperature,  $T_{max}$ , as a function of  $M_d$  and DR:  $T_{max} =$   
 163  $f(M_d, DR)$ , (Figure 4).

164 The knowledge of the fundamental mapping allowed fixing a relationship between the  
 165 maximum surface temperature and the moisture ratio in correspondence of a preselected  
 166 target value for the DR. On such basis, the LabView code was able to adjust the temperature  
 167 after on line measuring the actual weight i.e. the moisture ratio.

#### 168 *2.4 Chemical and physical analysis*

169 Malic acid, citric acid, glucose and fructose were determined by enzymatic kits (Boehringer  
 170 Mannheim, Germany), pH was measured with a glass-electrode pH-meter (Hanna  
 171 Instruments). Total phenols were determined with Folin-Ciocalteu reagent at 760 nm

172 (Cinquanta, Albanese, Fratianni, La Fianza & Di Matteo, 2013). Colour was obtained  
173 through a colorimeter Minolta Chroma Meter II Reflectance CR-400 (Cuccurullo et al.  
174 2012). Non-enzymatic browning was evaluated by the absorbance variation at 420 nm  
175 using Perkin Elmer, Lambda Bio 40 spectrophotometer. Texture of apple samples was  
176 measured by means of Texture Profile Analysis (Cuccurullo et al. 2017). Data were  
177 analysed by Bluehill 2 software package (Version 2.5, Instron Corporation, High  
178 Wycombe, UK). The rehydration of dried apple slices was carried out according to Atarés,  
179 Chiralt & González-Martínez (2009).

### 180 *Statistical analysis*

181 Chemical and physical analysis were performed in triplicate for all trials. Data reported are  
182 means and standard deviations calculated from three replicates. The analysis of variance  
183 (ANOVA) was applied to the data. The least significant differences were obtained using  
184 an LSD test ( $P < 0.05$ ). Statistical analysis was performed using an SPSS version 13.0 for  
185 Windows (SPSS, Inc., Chicago, IL, USA).

## 186 **3. Result and discussion**

### 187 *3.1. Preliminary experimental tests*

188 The recorded maximum temperature during experimental tests at 60 °C, 70°C and 80°C,  
189 are shown in Figure 5. Higher temperatures required longer times meanwhile the  
190 corresponding energy consumptions were roughly the same, as deduced by summing up all  
191 the time intervals were the magnetron was turned on (data not reported). The higher the  
192 temperature level, the higher temperature fluctuations resulted, probably owing to the  
193 reduction in dielectric loss factor with temperature (Cuccurullo et al. 2012). Moreover,  
194 temperature fluctuations become larger toward the end of the process when power density  
195 increased due to mass reduction. The standard deviations related to 60, 70 and 80 °C  
196 temperatures levels turned out to be 1.2, 1.6 and 2.2 °C respectively; these values were  
197 significantly below those recorded in a previous search because of the adoption of a mode  
198 stirrer (Cuccurullo et al. 2017).

### 199 *3.2 Drying rate control*

200 The maximum drying rate was arbitrarily chosen to be  $DR_{\max} = 0.003 \text{ s}^{-1}$  aiming to reduce  
201 thermal stress in the middle drying phase. Then, the control system started to modulate the  
202 magnetron delivered power according to the fundamental mapping previously identified,

203 i.e. suitably reducing the temperature level of the samples under test. The resulting drying  
204 rates are reported in Figure 6; the fitted drying-rate curves for the each preset temperature  
205 level are shown for reference, as well. The ability of the system to recover the target  $DR_{max}$   
206 is witnessed by the maximum relative error which is lower than 6.7% and by the RMSE  
207 which turns out to be  $9.9 \cdot 10^{-5} \text{ s}^{-1}$ .

208 Inspection of Figure 6 shows that adapting temperatures to reduce evaporation rates is  
209 effective within the first 22.1 minutes of the drying process, i.e. roughly after the middle  
210 stage completion: in fact, since the samples upper limit for temperature is fixed at  $80^{\circ}\text{C}$ , a  
211 time threshold is attained for which the maximum temperature remains unchanged at  $80^{\circ}\text{C}$ .  
212 Therefore, in the late stage of the drying process, evaporation rates slow down continuously  
213 following a path at constant temperature. The overall time needed to complete the test turns  
214 out to be 51.9 minutes, therefore the drying slows down with respect to the test @  $80^{\circ}\text{C}$  (-  
215 24.7%), however it is faster than the test @  $70^{\circ}\text{C}$  (+10.4%), which exhibits almost the same  
216 quality, as will be shown later. In Figure 7, the average and the maximum surface  
217 temperature evolution during drying process are reported. While progressively losing  
218 water content, holding constant the selected  $DR_{max}$  requires monotonically increasing the  
219 surface temperature of the samples under test. The modulation of the maximum surface  
220 temperature is evident: it is required in the first 22.1 minutes of the process, to reduce the  
221 high evaporation rates realized by operating at constant temperature. Then, when the  
222 samples upper limit for temperature is attained, the  $80^{\circ}\text{C}$ -constant temperature path is  
223 followed. Meanwhile, the sample average surface temperatures slightly decrease with time  
224 increasing, since the diminishing water mass determines higher generation rates and, in  
225 turn, higher temperature spans.

### 226 3.3. *Quality assessment*

227 The proximate composition of fresh apples (Table 2) showed a relevant content in  
228 polyphenols: about 140 ppm, as enzymatic browning is a consequence of phenolic  
229 compounds' oxidation by polyphenol oxidase, which triggers the generation of dark  
230 pigments. The constant drying rate did not affect the color of dried apples, measured by  
231 white index (WI), respect to references at controlled temperatures (Table 3). However, the  
232 browning caused by non-enzymatic browning, showed a significant decrease by operating  
233 at constant drying rate (Table 3). Texture is another important quality attribute of food  
234 products, at higher temperature ( $80^{\circ}\text{C}$ ), dehydrated apples showed a significant firmness  
235 increase (Table 3). A correlation between hardening of the apple and reduced rehydration

236 capacity (data not reported) was also found at 80°C. When the drying temperature is high,  
237 cell membranes rupture and release water into the extracellular space and therefore the  
238 transport of water to the outside occurs predominantly through the extracellular space  
239 (Halder, Dhall & Datta, 2011), causing a stiffening of the structure. On the other hand,  
240 the tests carried out at constant drying rate resulted in softer texture compared to the  
241 samples at 80°C.

#### 242 **4. Conclusions**

243 By a preliminary data reduction, a fundamental map with a relationship among the three  
244 main variables involved in the microwave drying process: the temperature level, the drying  
245 rate and the moisture ratio, was developed. A real time drying control system by a computer  
246 aided thermography system allowed switching on-off the magnetron to set an automatic  
247 control to adapt temperature level of the target apple slices so to realize fixed evaporation  
248 rates in the middle stage-drying period. The overall time needed to complete the drying  
249 process turned out to be comprised between the ones related to 70 and 80°C fixed  
250 temperature operations, but closer to the latter, ensuring finer product quality. In fact, a  
251 softening in apple slices dried with fixed evaporation rates was obtained respect to those  
252 dried at 80°C.

253

#### 254 **5. References**

- 255 Atarés, L., Chiralt A., & González-Martínez, C. (2009). Effect of the impregnated solute  
256 on air drying and rehydration of apple slices (cv. *Granny Smith*). *Journal of Food*  
257 *Engineering*, 91, 2, 305-310.
- 258 Chayjan, R. A., & Alaei, B. (2013). Characteristics of thin layer microwave drying of  
259 apricot. *Electronic Journal of Polish Agricultural Universities*, 16, 12.
- 260 Cinquanta, L., Albanese D., Fratianni A., La Fianza G., & Di Matteo M. (2013).  
261 Antioxidant activity and sensory attributes of tomatoes dehydrated by combination  
262 of microwave and convective heating. *Agro Food Industry Hi-Tech*, 24, 35-38.
- 263 Clark, D. E. (1996). Microwave processing of materials. *Annual Review of Materials*  
264 *Science*, 26, 299-331.

- 265 Cuccurullo, G., Giordano, L., Albanese, D., Cinquanta, L. & Di Matteo, M. (2012).  
266 Infrared thermography assisted control for apples microwave drying, *Journal of*  
267 *Food engineering*, 112, 319-325.
- 268 Cuccurullo, G., Giordano, L., Metallo, A. & Cinquanta, L. (2017). Influence of mode stirrer  
269 and air renewal on controlled microwave drying of sliced zucchini, *Biosystems*  
270 *engineering* 158, 95-101.
- 271 Gunasekaran, S. (1999). Pulsed microwave-vacuum drying of food materials. *Drying*  
272 *Technology*, 17(3), 395-412.
- 273 Halder, A. A., Dhall & Datta, A. K. (2011). Modeling transport in porous media with phase  
274 change: Applications to food processing. *Journal of Heat Transfer, Transactions of*  
275 *the American Society of Mechanical Engineers*. 133(3): 031010-1–031010-13.
- 276 Karaaslan, S. N., & Tuncer, I. K. (2008). Development of a drying model for combined  
277 microwave fan-assisted convection drying of spinach. *Biosystems Engineering*, 1,  
278 44-52.
- 279 Koné, Y. K., Druon, C., Etienne, D., Gnimpieba, Z., Delmotte, M., Duquenoy, A. &  
280 Laguerre, J. C. (2013). Power density control in microwave assisted air drying to  
281 improve quality of food, *Journal of Food engineering*, 4, 750-757.
- 282 Maskan, M. (2000). Microwave/air and microwave finish drying of banana. *Journal of*  
283 *Food Engineering*, 44, 71-78.
- 284 Nijhuis, H. H., Torringa, H. M., Muresan, S., Yuksel, D., Leguijt, C., & Kloek, W. (1998).  
285 Approaches to improving the quality of dried fruit and vegetables. *Trends in Food*  
286 *Science and Technology*, 9, 13-20.
- 287 Raghavan, G. S. V., Zhenfeng, L., Wang, N. & Gariépy, Y. (2010). Control of  
288 Microwave Drying Process Through Aroma Monitoring, *Drying Technology*, 28, 5,  
289 591-599.
- 290 Wang, J., Xiong, Y.-S., & Yu, Y. (2004). Microwave drying characteristics of potato and  
291 the effect of different microwave powers on the dried quality of potato. *European*  
292 *Food Research Technology*, 219, 500-506.

293 Zhenfeng, L., Wang, N., Raghavan, G. S. V. & Cheng W. (2006). A microcontroller-based,  
294 feedback power control system for microwave drying processes, *Applied engineering*  
295 *in Agriculture*, 22, 309-314.

296 Zhenfeng, L., Raghavan, G. S. V. & Wang, N. (2010). Carrot volatiles monitoring and  
297 control in microwave drying, *LWT - Food Science and Technology*, 43 291-297.

298 Zhenfeng, L., Raghavan, G. S. V., Wang, N. & Vigneault, C. (2011). Drying rate control  
299 in the middle stage of microwave drying, *Journal of Food engineering*, 2, 234–238.

300

301

302

### 303 **Figures captions**

304 **Figure 1.** Schematic diagram of the microwave lab plant drying system.

305 **Figure 2.** Drying curves of apple slices during microwave heating at 60, 70 and 80 °C.

306 **Figure 3.** Drying rate curves during microwave drying of apples slices at 60, 70 and 80°C.

307 **Figure 4.** The fundamental mapping: linear interpolation among the maximum surface  
308 temperature ( $T_{\max}$ ) of apples slices during microwave drying, as a function of moisture  
309 content on dry basis ( $M_d$ ) and drying rate (DR).

310 **Figure 5.** Temperature fluctuations upon apple slices detected by infrared thermography  
311 during microwave heating at constant temperature (60, 70 and 80 °C).

312 **Figure 6.** Drying rates (DR) of apple slices as a function of moisture content on dry  
313 basis ( $M_d$ ) during controlled drying rate tests (●). The vertical bars indicate the standard  
314 deviation.

315 **Figure 7.** Maximum and average surface temperature evolution upon apple slices during  
316 a controlled drying rate test

317

318

319

320

321

322

323

324  
325  
326  
327  
328

329 Table 1. List of the fitting parameters used in this work and related fit quality. RSME (root mean  
330 square error); DR (drying rate),  $M_d$  (moisture content on dry basis).

Temperature [°C]	a	-b	c	d	e	Drying time [min]	RMSE	
							DR [s <sup>-1</sup> ]	$M_d$ [-]
60	1.62 10 <sup>-04</sup>	1.71 10 <sup>-03</sup>	2.53 10 <sup>-03</sup>	1.64	9.76 10 <sup>-02</sup>	80.1±4.3	6.4 10 <sup>-5</sup>	4.67 10 <sup>-2</sup>
70	2.16 10 <sup>-04</sup>	2.33 10 <sup>-03</sup>	6.19 10 <sup>-03</sup>	1.57	1.62 10 <sup>-01</sup>	57.9±2.3	8.6 10 <sup>-5</sup>	8.63 10 <sup>-2</sup>
80	3.83 10 <sup>-04</sup>	3.16 10 <sup>-03</sup>	1.51 10 <sup>-02</sup>	1.54	2.68 10 <sup>-01</sup>	41.6±3.3	13.3 10 <sup>-5</sup>	5.04 10 <sup>-2</sup>
variable						51.9±3.6	9.9 10 <sup>-5</sup>	

331  
332  
333

334 Table 2. Proximate composition (%) of fresh apples

Water	85.6 ± 0.7
Sugar	12.4± 0.3
pH	4.1± 0.1
Phenols*	140.2± 8.2
Citric acid	0.12± 0.02
Malic Acid	0.18± 0.03

335 \*ppm of catechin

336  
337

338 Table 3 - White index (WI), non-enzymatic browning (NEB) and hardness (N) in fresh and  
339 apples dried at different temperatures (60, 70 and 80°C) and at constant evaporation rate  
340 (CER).

Parameter	Fresh samples	Dried samples:			
		60°C	70°C	80°C	CER
WI	69.2 <sup>a</sup>	46.9 <sup>b</sup>	48.9 <sup>b</sup>	50.7 <sup>b</sup>	48.5 <sup>b</sup>
NEB	0.05 <sup>a</sup>	0.28 <sup>b</sup>	0.30 <sup>b</sup>	0.26 <sup>b</sup>	0.21 <sup>c</sup>
Hardness	0.5 <sup>a</sup>	2.8 <sup>b</sup>	2.5 <sup>b</sup>	3.5 <sup>c</sup>	2.7 <sup>b</sup>

341 Unequal letter within same row indicate significant differences ( $P < 0.05$ )  
342 (standard deviation are not reported because below 5%)  
343



