

1 **Production of Antimicrobial Membranes Loaded with Potassium Sorbate using**
2 **a Supercritical Phase Separation Process**

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9 **Abstract**

10 The production of antimicrobial active packaging is one of the most **interesting** challenges in
11 the food industry; its scope is to prolong the shelf-life of a food maintaining its safety and freshness.
12 The major limitation of traditional techniques used to produce antimicrobial packaging, is the
13 difficulty in controlling the release of the active agent from the device to the food surface.

14 In this work, a supercritical phase inversion process has been tested to produce Potassium
15 Sorbate (PS) loaded Cellulose Acetate (CA) membranes, to be inserted in food packaging. The
16 antimicrobial membranes have been obtained at different process conditions (pressures 150-250 bar,
17 temperatures 35-55 °C) **and at different polymer concentrations (10, 15 and 20% w/w). PS to CA**
18 **weight ratio has been maintained constant at 5% w/w for all the formulations. The produced**
19 **membranes** have been characterized from a chemico-physical point of view and PS release tests
20 have been performed. The best **process parameters** combination to obtain the longest PS release
21 time (about 325 min) was 250 bar and 35 °C for 20% w/w CA membranes.

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23
24 **Keywords:** Cellulose acetate, Potassium sorbate, Antimicrobial membranes, Phase separation,
25 Supercritical CO₂.

26 1 Introduction

27 The production of antimicrobial active packaging is one of the most **interesting** challenges in
28 the food industry. Its scope is to prolong the shelf-life of a food and to maintain its safety and
29 freshness. Traditionally, antimicrobial agents are directly mixed with the food formulation; but, it is
30 difficult to control the agent activity and selectivity, due to the reactions with the food components
31 (Appendini & Hotchkiss, 2002; Min & Krochta, 2005). An alternative to this process, can be the
32 use of antimicrobial devices and antimicrobial films, inserted in the food packaging.

33 Some characteristics are required for the effectiveness of an active packaging; in particular, a
34 suitable concentration and a proper release rate of the active agent to avoid burst effects or a too
35 slow release (Appendini & Hotchkiss, 2002; Vermeiren et al., 1999).

36 Scientific literature reports several techniques to produce antimicrobial packaging (Appendini
37 & Hotchkiss, 2002; Cha & Chinnan, 2004; Vermeiren et al., 1999): 1) sachets containing volatile
38 antimicrobial agents; 2) incorporation of volatile and non-volatile antimicrobial agents directly into
39 polymers; 3) coating or adsorption of antimicrobials onto polymer surfaces; 4) immobilization of
40 antimicrobials on polymers by ion or covalent linkages; 5) use of antimicrobial polymers.

41 The major limitation of all the proposed methods, is the difficulty in controlling the release of
42 the active agent from the device to the food surface. Some authors tried to overcome this problem
43 using multilayer films containing an active agent (Buonocore et al., 2005; Mastromatteo et al.,
44 2009; Mastromatteo et al., 2010; Uz & Altinkaya, 2011) or producing films loaded with the
45 antimicrobial agent (Gemili et al., 2009; Tankhiwale & Bajpai, 2012). But, they had the problem of
46 cross-linking the polymer to prolong the release of the active compound. In the case of membrane-
47 like processes, an asymmetric porous structure was produced by evaporation of the organic solvent
48 (Gemili et al., 2009). Using this process, it is difficult to control membrane morphology, since the
49 operative parameters are temperature and humidity only.

50 Potassium Sorbate (PS) is a potassium salt of the sorbic acid, well-known for its potential
51 antifungal activity (Mehyar et al., 2014; Sayanjali et al., 2011b; Valencia-Chamorro et al., 2008). It

52 has been used to inhibit the growth of molds and yeasts; but, it is active also against *Staphylococcus*
53 *aureus*, *Clostridium botulinum*, salmonellae and pseudomonads (Zamora & Zaritzky, 1987). Its
54 stability is not a problem; but, its release is problematic. Sayanjali et al. (2011) produced by solvent
55 evaporation, carboxymethyl cellulose based-edible film containing PS as antimicrobial agent. They
56 demonstrated the efficacy of the antimicrobial film against *A. parasiticus* and *A. flavus*. Moreover,
57 they coated pistachios with this film, obtaining molds growth inhibition (Sayanjali et al., 2011a).
58 Basch et al. (2013) studied the antimicrobial effectiveness of nisin and PS incorporated in films
59 produced by solvent evaporation technique of tapioca starch and its mixtures with hydroxypropyl
60 methylcellulose. They verified that the combination of antimicrobials was more effective against
61 *Listeria innocua* and *Zygosaccharomyces bailii*, than their individual incorporation (Basch et al.,
62 2013).

63 However, in these studies, the authors produced dense films. Therefore, the active agent
64 release and its action were reduced by the large mass transfer resistance in the polymer matrix.
65 Moreover, solvent evaporation technique can produce the deposition of the active agent on the
66 bottom surface of the film due to the slowness of the process, changing film performance in
67 dependence of which surface is in contact with food.

68 To overcome conventional processes limitation, it could be possible to use supercritical
69 assisted processes, taking advantage of the properties of supercritical fluids, such as negligible
70 surface tension, high diffusivity and low viscosity. These characteristics have been already
71 successful used to produce micro- and nano-particles, in pharmaceutical, food and biomedical field
72 (Campardelli et al., 2015; Della Porta et al., 2013; Garofalo et al., 2014; Liparoti et al., 2015;
73 Prosapio et al., 2014; Reverchon & Adami, 2013; Espirito Santo et al., 2014), in the separation
74 and/or the extraction of natural compounds (De Melo et al., 2014).

75 A supercritical phase separation process has been proposed to produce loaded polymeric
76 membranes; the literature shows that this process is more versatile with respect to the traditional
77 ones, since changing operative conditions (i.e., pressure and temperature) it is possible to influence

78 kinetics and thermodynamics of the process (Reverchon & Cardea, 2004). It has been previously
79 adopted to produce membranes loaded with a catalyst (Cardea & Reverchon, 2011), a drug (Cardea
80 et al., 2014a; Cardea et al., 2014b; Cardea et al., 2010) and biological compounds for food
81 applications (Baldino et al., 2014).

82 Therefore, the aim of this work is to use the supercritical phase inversion process to produce
83 PS loaded membranes to be inserted in food packaging. Cellulose acetate (CA) has been selected as
84 the polymer, since it is allowed by the Food and Drug Administration (FDA) for food contact. **The**
85 **antimicrobial membranes will be characterized from a chemico-physical point of view and PS**
86 **release tests will be performed to evidence the effect of the membranes morphology on the kinetics**
87 **of the active agent release.**

88

89 **2 Materials and Methods**

90 Cellulose acetate, CA, (average M_n ca. 50000 with acetyl content of 39.7%), Acetone (purity
91 99.5%) and Potassium sorbate (the raw material is shown in Figure 1), PS, (purity 99.0%) were
92 bought from Sigma-Aldrich (Milan, Italy); CO₂ (purity 99%) was purchased from Eurossigeno
93 (Napoli, Italy). Distilled water was produced in our laboratory using an ISCO mod. AUTOSTILL
94 DST/5. All materials were processed as received.

95

96 **2.1 Antimicrobial membranes preparation**

97 **Polymer solutions were prepared dissolving CA in Acetone at 40 °C for 24 h. At the same**
98 **time, a solution containing PS and water was prepared in an Eppendorf container under Vortex**
99 **shaking at room temperature for 5 min; then, the two solutions (CA-Acetone and PS-water) were**
100 **mixed for 1 h. CA amount varied between 10 and 20% w/w in Acetone and the PS amount ranged**
101 **between 10 and 20% w/w in water; the ratio between CA-Acetone and PS-water solutions was**
102 **maintained constant at 95:5. These weight percentages are summarized in Table 1. The solutions**
103 **were distributed on stainless steel caps, having a diameter of 2 cm and a height of about 1 mm, and,**

104 then, processed by Supercritical phase separation at different process conditions: temperatures
105 ranging between 35 and 55 °C and pressures ranging between 150 and 250 bar.

106 Antimicrobial membranes were produced in a home-made laboratory apparatus previously
107 described (Reverchon et al., 2004). The caps were rapidly put inside the high pressure vessel (a 316
108 stainless steel vessel with an internal volume of 80 mL) to minimize evaporation of the solvent. The
109 vessel was closed and filled with SC-CO₂ up to the desired pressure, using a high pressure pump
110 (mod. LDB1, Lewa, Germany). Pressure in the vessel was measured by a test gauge (mod. MP1,
111 OMET, Italy) and regulated using a micrometering valve (mod. 1335G4Y, Hoke, USA).
112 Temperature was regulated using PID controllers (mod. 305, Watlow, USA). At the exit of the
113 vessel, a rotameter (mod. D6, ASA, Italy) was used to measure CO₂ flow rate, that was maintained
114 constant at 1.5 Kg/h.

115

116 **2.2 Antimicrobial membranes characterization**

117 *2.2.1 Field Emission Scanning Electron Microscopy (FESEM)*

118 Antimicrobial membranes were cryofractured using liquid Nitrogen (SOL, Milan, Italy); then,
119 the samples were sputter coated with gold (Agar Auto Sputter Coater mod. 108 A, Stansted, UK) at
120 30 mA for 150 s and analyzed by a FESEM (mod. LEO 1525, Carl Zeiss SMT AG, Oberkochen,
121 Germany), used to study membrane morphology.

122

123 *2.2.2 Membrane pore size analysis*

124 Sigma Scan Pro 5.0 (Jandel Scientific, San Rafael, Canada) and Origin 8.5 (Microcal,
125 Northampton, USA) softwares were used to determine the average diameter of membrane pores.
126 Images taken at various locations in the membrane were used for each calculation. We measured
127 about 300 pores for each sample analyzed. Using Origin software, we first represented an histogram
128 with the percentage of the pores having a given diameter; then, we performed a curve fitting to
129 obtain the pore size distribution curve.

130

131 2.2.3 Membranes porosity

132 The porosity (ε) represents the “void space” of the membrane and was calculated from the
133 density of the membrane and the density of untreated CA:

$$134 \quad \varepsilon = 1 - \frac{\rho_{memb}}{\rho_{CA}}$$

135 The membrane density was determined by measuring its volume and weight:

$$136 \quad \rho_{memb} = \frac{\text{Membrane weight}}{\text{Membrane volume}}$$

137 The membrane volume was obtained using the Archimede’s principle: the membrane was
138 waterproofed and subsequently immersed in pure water. Calculating the weight of the displaced
139 water, we measured the volume of the sample. The presence of PS was neglected in this calculation.

140 **Five specimens were tested for each sample.**

141

142 2.2.4 Differential scanning calorimetry (DSC)

143 DSC (DSC 30 Mettler, Toledo) was carried out to analyze and identify any changes in the
144 thermograms of pure substances compared to polymer/preservative formulations.

145 Calorimetric analysis was performed in the temperature range between -60 and 300 °C, with a
146 heating rate of 10 °C/min; the inert gas was Nitrogen, with a flow rate of 50 L/min.

147

148 2.2.5 Energy dispersive X-ray spectroscopy (EDX)

149 Antimicrobial membranes were cryofractured using liquid Nitrogen and sputter coated with
150 Chromium (EMITECH K575X peltier cooled). They were analyzed by EDX (INCA Energy 350,
151 Oxford Instruments) to observe the components distribution in the sample; in particular, Potassium
152 atoms were selected for PS and Carbon atoms for CA.

153

154 2.2.6 X-Ray analysis

155 X-Ray diffractograms were recorded using an X-ray powder diffractometer (mod. D8
156 Discover, Bruker AXS, Inc., USA) with a Cu sealed tube source. The measuring conditions were:
157 Ni-filtered CuK α radiation, $\lambda = 1.54 \text{ \AA}$, 2θ angle ranging from 5° to 60° with a scan rate of 1 s/step
158 and a step size of 0.037° .

159

160 2.2.7 Potassium sorbate release test

161 PS release kinetics were determined measuring the increase of active agent concentration in
162 distilled water at room temperature. The antimicrobial membrane was placed in a bottle containing
163 50 mL of water, that simulate the food environment, and stirred at 50 rpm. To determine the PS
164 release rate from the membrane and its concentration, analysis was carried out in continuous using a
165 Varian (mod. Cary 50) UV/Vis spectrophotometer and reading the absorbance of the sample at 254
166 nm (that is the wavelength at which PS shows maximum absorption).

167

168 3 Results and Discussion

169 3.1 Effect of process parameters on antimicrobial membranes morphology

170 In the first part of the work, we studied the effect of PS incorporation in CA membranes to
171 explore the possible interferences of solubilized PS on membranes morphology. Therefore, CA
172 membranes at 10, 15 and 20% w/w in Acetone, loaded with PS at 5% w/w with respect the
173 polymer, were prepared. We also analyzed the effect of SC-CO $_2$ solvent power, performing
174 experiments at low, medium and high SC-CO $_2$ density, corresponding to 150 bar 55 °C ($\rho_{\text{CO}_2} = 0.66$
175 g/cm 3), 200 bar 45 °C ($\rho_{\text{CO}_2} = 0.81 \text{ g/cm}^3$) and 250 bar 35 °C ($\rho_{\text{CO}_2} = 0.90 \text{ g/cm}^3$), respectively.
176 Indeed, the solvent power of SC-CO $_2$ is a function of its density, that increases with pressure and
177 decreases with temperature.

178 Summarizing the results, at all the operative conditions tested, CA membranes maintained the
179 shape and volume of the starting solutions. A macroscopic example of the final membrane is
180 depicted in Figure 2.

181 The observation at macroscopic level confirms that shrinkage phenomena were avoided
182 during the supercritical process. When traditional phase separation processes are used, instead, the
183 final membrane structure can collapse due to the surface tension of the liquid system on the polymer
184 matrix, leading to a membrane with a reduced volume.

185 In Figure 3, FESEM images, taken at different enlargements, of the section of the
186 antimicrobial membranes at 10, 15 and 20% w/w CA, processed at 200 bar and 45 °C (medium SC-
187 CO₂ solvent power) are reported.

188 The morphology of the membranes is similar to the ones obtained in a previous work on CA
189 membranes (Reverchon et al., 2004), where CA-Acetone solutions were processed at pressures and
190 temperatures ranging between 100 and 200 bar and 45 - 65 °C, respectively. This comparison is
191 relevant, since it means that the presence of water, used to dissolve PS, does not interfere with the
192 SC-CO₂ induced phase separation of the CA-Acetone system. This result was not obvious, since it
193 is well known that, differently from Acetone, water at the usual phase separation conditions, shows a
194 very reduced affinity with SC-CO₂ and, therefore, its presence could interfere or modify the phase
195 separation process and the produced morphologies.

196 Summarizing the information in Figure 3, membranes structure varied from finger-like to
197 cellular, increasing CA concentration from 10 to 20% w/w. CA membranes at 15 and 20% w/w
198 were characterized by an uniform cellular morphology, in which the mean pore size decreased from
199 about 8 to 5 μm, increasing CA amount from 15 to 20% w/w, respectively. The same results were
200 observed at all tested process conditions; i.e., also when different pressures and temperatures were
201 used. The mean pore size measured for each membrane is reported in Table 2.

202 To explain these results, it is possible to refer to the classical phase separation theory (Van de
203 Witte et al., 1996) and previous works on membranes formation by supercritical phase separation
204 (Reverchon et al., 2004). At 10% w/w CA, a spinodal decomposition occurred and a fingers-like
205 morphology was obtained (Stropanik & Kaiser, 2002); at 15 and 20% w/w CA, the nucleation and

206 growth of the polymer poor-phase within the polymer rich-phase occurred, producing a cellular
207 structure.

208 Comparing the pore size distribution curves showed in Figure 4 and the related data in Table
209 3, we observed that, maintaining a constant CA concentration (e.g., 15% w/w), and varying process
210 conditions (T/p, °C/bar: 55/150, 45/200, 35/250), the mean pore size decreased and pore size
211 distribution sharpened. This is a consequence of SC-CO₂ density increase from about 0.66 to 0.90
212 g/cm³, and, as previously indicated, of the increase of solvent power that influences the phase
213 separation kinetics. When SC-CO₂ solvent power increases, phase separation process becomes
214 faster and the lean polymer phase has not time enough to grow in the polymer rich phase. As
215 consequence, membrane structure is characterized by smaller pore size and pore size distribution is
216 sharper (Reverchon et al., 2004).

217 This series of experiments demonstrated that the presence of the preservative (i.e., PS) and
218 water, did not influence the CA membrane formation process from a kinetic and a thermodynamic
219 point of view.

220 When we observed the CA matrix at higher FESEM enlargements, we noted that PS is clearly
221 detectable as precipitated and encapsulated microparticles (Figure 5); whereas, before the process,
222 PS was a powder with an irregular shape of about 1 mm (see Materials and Methods section). Small
223 quantities of PS microparticles were distributed on the CA membrane surface; this phenomenon is
224 particularly evident for the 10% w/w CA membranes.

225 This is the first time that microparticles formation has been obtained during SC-CO₂ phase
226 inversion; i.e., simultaneous polymer phase separation and micronization of the active principle
227 during the same experiment. This is a relevant further information on the composite membrane
228 formation mechanism: solubilized PS has been released from the Acetone+water+CA solution by a
229 sort of supercritical antisolvent precipitation mechanism, largely used in the so-called SAS process
230 (Supercritical AntiSolvent micronization) (De Marco et al., 2015; Reverchon & De Marco, 2011).
231 This process is for some aspects similar to SC-phase separation; but, in the case of PS, it produced

232 microparticles, instead of PS participation during the formation of the continuous structure of the
233 polymeric membrane. The fact that the particles are only partly incorporated in the polymer,
234 indicates that they precipitated from the liquid phase, when the polymeric structure was already
235 formed.

236 To explain this phenomenon, we have first to consider the preparation step of the samples and
237 the kind of system formed by PS and CA. In particular, PS was dissolved in water and, then, added
238 to the CA-Acetone solution, since PS is not soluble in this organic solvent. During the supercritical
239 assisted process, SC-CO₂ can form a supercritical mixture with Acetone (Reverchon et al., 2004);
240 whereas, SC-CO₂ and water show a very limited affinity (Sabirzyanov et al., 2002). Therefore,
241 Acetone is rapidly eliminated during phase separation and it is very probable that part of water (in
242 which PS tends to concentrate) is eliminated near the end of the process: only at this point, PS
243 precipitates in form of microparticles that can fall in the empty spaces formed by membrane pores.
244 This hypothesis could also justify why this phenomenon was mainly observed for 10% w/w CA
245 membranes. Indeed, in that case, due to the minor amount of polymer, the entrapment capacity of
246 the CA matrix was more limited.

247

248 **3.2 DSC and EDX analyses**

249 DSC analysis was performed to compare CA and PS thermograms with those of the
250 polymer/PS formulations to identify eventual modifications of the processed materials. CA
251 thermogram, in Figure 6, shows that the polymer glass transition temperature is located at about 78
252 °C and its melting temperature is about 237 °C. PS thermogram has a minimum at about 160 °C,
253 which corresponds to its melting temperature.

254 Looking at thermograms of the antimicrobial membranes, the characteristic of CA were
255 preserved, also at larger polymer concentration; whereas, PS fusion peak was no more detectable. It
256 probably means that due to the fast supercritical processing, PS precipitated in an amorphous form.

257 This behavior was already observed in the case of Amoxicillin loaded in Poly(vinylidene fluoride)
258 aerogels for pharmaceutical applications (Cardea et al., 2011).

259 This result confirms the encapsulation and the micronization of PS in CA, since the polymer
260 matrix blocks PS reorganization in a more ordinate form (i.e., the crystalline state).

261 We also analyzed the antimicrobial dispersion inside the polymer matrix by EDX. In Figure 7,
262 element maps identifying CA and PS in a membrane at 15% w/w CA processed at 200 bar and 45
263 °C are reported. In particular, we selected Carbon atoms for CA and Potassium atoms for PS. As
264 shown in the pictures, PS (in red) was uniformly distributed in CA membrane (in green), since the
265 area in which Potassium was detected totally overlaps the Carbon area.

266 Moreover, we also verified by EDX that detected microparticles were formed by PS, as
267 reported in Figure 8. In particular, this figure shows the EDX signal of a single microparticle
268 selected from those observed in the previous FESEM image (see Figure 5).

269 Therefore, these analyses confirm that we produced antimicrobial membranes in which the
270 active principle was dispersed in the polymer matrix and, at 10% w/w CA, a small part of it also
271 precipitated on the membrane external surface.

272

273 **3.3 X-Ray analysis**

274 X-Ray analyses were performed to confirm PS solid state after the supercritical phase
275 separation process, as hypothesized in the results of DSC analysis. In Figure 9, we compared the X-
276 ray diffraction patterns of the raw materials with the CA+PS physical mixture and the CA+PS
277 membrane. As expected, PS is crystalline, CA is semi-crystalline and their physical mixture
278 maintained some peaks of the two compounds. The X-ray diffraction pattern of CA+PS membrane
279 shows instead that the sample is substantially amorphous.

280

281 **3.4 PS release tests from CA membranes**

282 Differently from the case of antimicrobial principles based on bioactive compounds (for
283 example, an enzyme), PS stability is not a concern; therefore, activity tests were not performed. In
284 this case, the most relevant characteristic to be measured, is the release rate of PS from CA
285 membranes in water. Water is generally used as the medium to simulate a food (Buonocore et al.,
286 2005; Uz & Altinkaya, 2011). Using the procedure described in Section 2.2.7, we tested the
287 membranes at 10, 15 and 20% w/w CA processed at different SC-CO₂ solvent power. PS
288 concentration (C_t) was normalized to the maximum detected PS concentration (C_{inf}) to allow the
289 comparison among the curves, reported in Figure 10a-c. The aim of this analysis was to identify the
290 parameters influencing the performance of the antimicrobial membrane with respect to PS release
291 and the time required to achieve the maximum PS concentration in the medium.

292 The release curves showed an exponential trend for all samples tested; therefore, the release
293 mechanism was the same and was reproducible for the different membranes, even changing CA
294 concentration and the process operative conditions. A diffusion controlled mechanism can be
295 hypothesized (Uz & Altinkaya, 2011) when these trends are observed.

296 PS release rate decreased with CA concentration at all operative condition tested; this result
297 was expected considering that, increasing the polymer concentration, the membranes morphology
298 changed (from macrovoids to cellular one) and the pore size decreased (Figure 2). Moreover, a
299 slight burst effect can be observed in 10% w/w CA membranes; this phenomenon can be related to
300 the presence of the precipitated PS microparticles, as previously discussed, on the CA membrane
301 external surfaces, that make them easily available for a fast dissolution.

302 In Table 4, we reported the time required to achieve the maximum PS concentration for each
303 sample. As expected, PS release rate decreased for the membranes produced at higher SC-CO₂
304 solvent power; e.g., for the membranes processed at 250 bar/35 °C. In Figure 10c, the maximum PS
305 concentration was obtained after 75, 200 and 325 min for 10, 15 and 20% w/w CA, respectively.
306 This result is consistent with the measured porosity values (Table 3) and with the decrease of the
307 mean pores size (Figure 3), observed increasing the SC-CO₂ solvent power: smaller pores

308 determined a decrease of mass transfer coefficient of water and of PS+water solution inside the
309 membranes; i.e., more compact membranes lead to a slower PS release.

310 The maximum concentration of PS in water is not equivalent to a data about the duration of
311 the antimicrobial control exerted by the membrane. Indeed, the length of the preservative action will
312 depend on the quantity of microorganisms that is present in water and by the lithic action required.
313 Therefore, the measured release times have to be interpreted as the readiness of the membrane to
314 exert its antimicrobial action.

315 We also measured the maximum PS concentration released from CA membranes. In Table 5,
316 it is possible to observe as increasing the amount of CA in the polymer solutions (i.e., increasing the
317 amount of PS), the maximum concentration of PS increases, too. Moreover, for all the membranes
318 generated, the Minimal Inhibitory Concentration (MIC) for bacteria, that ranges from 15.7 - 250
319 mg/L (Gunes et al., 2013), was overcome. This aspect is very relevant for the application in active
320 packaging.

321 The process conditions did not affect the maximum PS concentration, that only depends on
322 the amount of PS in the starting solutions; on the other hand, the SC-CO₂ solvent power affects the
323 rate of PS release up to the maximum concentration, as previously observed in Table 4.

324

325 **4 Conclusions**

326 Different CA membranes loaded with PS were successfully produced by supercritical phase
327 separation and micronization of the active principle was simultaneously obtained. This result allows
328 to use these membranes in two ways: if a strong and fast microorganisms inhibition is required, the
329 membrane at lower polymer content is preferable, since PS release is faster; the other possibility is
330 to use membranes at higher polymer content, prolonging the inhibition effect and the safety of the
331 food.

332 Interpreting the results, the best combination to obtain the longest PS release time is the
333 maximum SC-CO₂ solvent power and the maximum CA concentration, that in this work
334 corresponds to the CA membrane at 20% w/w, obtained at 250 bar and 35 °C.

335

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440

441 **Figure Captions**

442 **Figure 1.** Untreated potassium sorbate powder.

443 **Figure 2.** Pictures of an antimicrobial CA membrane processed by Supercritical phase separation at
444 200 bar and 45 °C.

445 **Figure 3.** FESEM images of the section of antimicrobial CA membranes produced at 200 bar and
446 45 °C and at different CA concentrations: (a) 10% w/w, (b) 15% w/w, (c) 20% w/w, and at a
447 constant ratio PS/CA=5% w/w.

448 **Figure 4.** Pore size distribution of antimicrobial membranes at 15% w/w CA, processed at different
449 SC-CO₂ solvent power.

450 **Figure 5.** FESEM image showing PS microparticles partly encapsulated in the CA 10% w/w
451 matrix.

452 **Figure 6.** Thermograms of CA, PS and CA plus PS membranes processed at 200 bar, 45 °C.

453 **Figure 7.** EDX analysis of the antimicrobial membrane at 15% w/w CA processed at 200 bar, 45
454 °C: a) Potassium atoms; b) Carbon atoms.

455 **Figure 8.** EDX analysis of a microparticle formed inside the 10% CA membrane: a) FESEM
456 picture; b) Potassium atoms; c) Carbon atoms.

457 **Figure 9.** X-Ray analysis of PS, CA, CA+PS membrane and CA+PS physical mixture.

458 **Figure 10.** PS release curves from CA membranes at 10, 15 and 20% w/w in water, processed at: a)
459 150 bar, 55 °C; b) 200 bar, 45 °C; c) 250 bar, 35 °C.

460

461 **Table Captions**

462 **Table 1.** Weight percentages of each component used for the samples preparation.

463 **Table 2.** Mean pore size of antimicrobial membranes section.

464 **Table 3.** Porosity of the antimicrobial membranes phase separated at 150/55, 200/45, 250/35 p/T.

465 **Table 4.** Time to reach the maximum PS concentration changing SC-CO₂ solvent power.

466 **Table 5.** Maximum PS concentration released from CA membranes obtained at different SC-CO₂

467 solvent power.